



# Development of Stable Two-Way Shape Memory Behavior in a Polycrystalline NiTi Shape Memory Alloy



**O. Benafan, S.A. Padula II, R.D. Noebe, A. Garg, D.J. Gaydosch  
and G.S. Bigelow**

*Structures and Materials Division  
NASA Glenn Research Center*



**R. Vaidyanathan and D.E. Nicholson**

*Advanced Materials Processing and Analysis Center  
Mechanical, Materials and Aerospace Engineering Department  
University of Central Florida*



**T.A. Sisneros, B. Clausen and D.W. Brown**

*Los Alamos Neutron Science Center  
Los Alamos National Laboratory*



# Acknowledgment

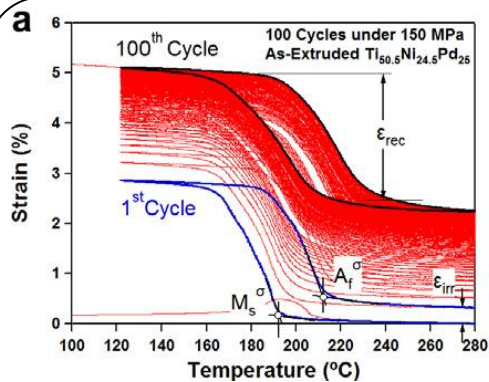
- **NASA Fundamental Aeronautics Program, Supersonics and Fixed-Wing Programs**
- **Basic Energy Sciences (DOE)**
- **CAS MART**



# Two-Way Shape Memory Effect (TWSME)

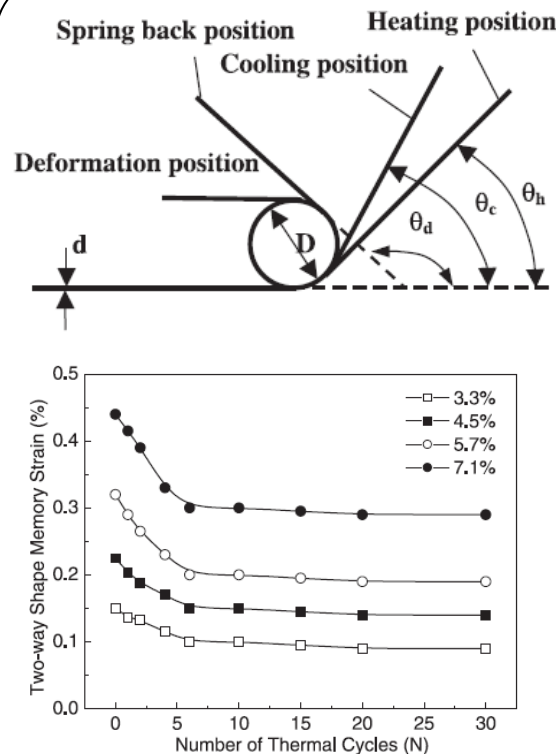
- Two-Way Shape Memory effect (TWSME) is not an inherent behavior of SMAs
- Can be obtained after specific thermomechanical training procedures (many different training methods have been developed)

## Thermomechanical cycling



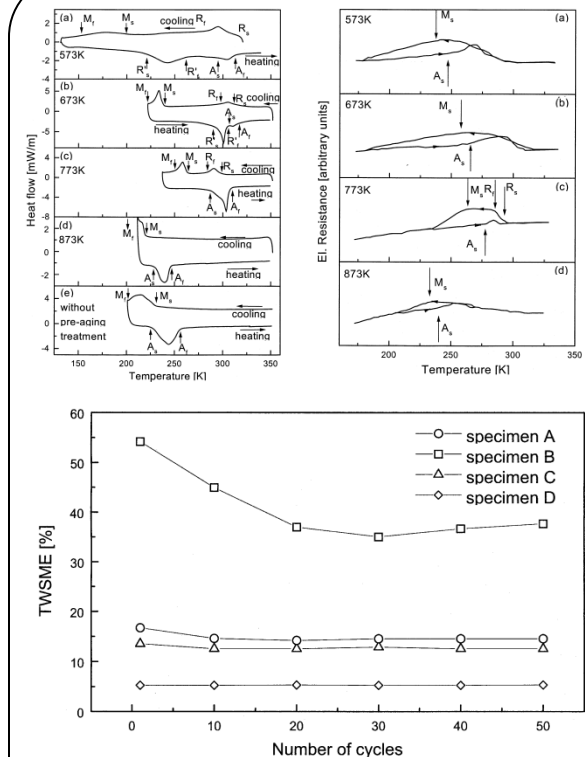
[1] K. C. Atli et al. / Scripta Materialia 65 (2011) 903–906

## Martensite deformation



[2] X.L. Meng et al. / Materials Letters 57 (2003) 4206–4211

## Precipitation/aging



[3] C.-Y. Chang et al. / Metall. Mater. Trans. A 32 (2001) 1629



# Motivation and Objectives

## Motivation:

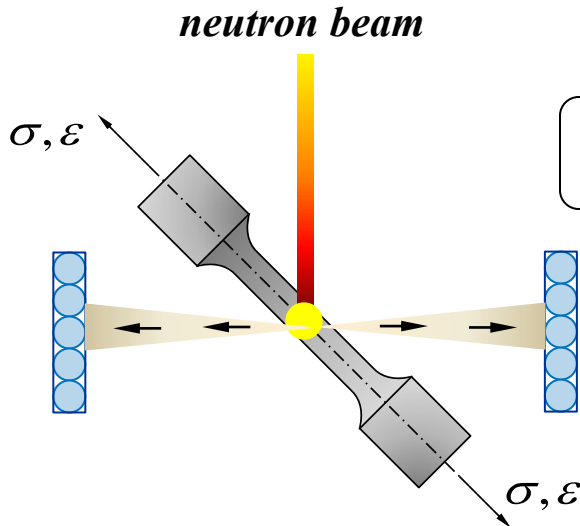
- Training by martensite deformation is relatively easy and quick [4] Y. Liu et al./Acta Mater. 47, (1998)
- Requires little more than a onetime deformation of the material
- Multiple thermomechanical cycles are NOT REQUIRED

## Objectives:

- Investigate the role of deformation on the stability and efficacy of the TWSME
- Examine the micromechanical and microstructural changes associated with the training procedure (neutron diffraction)
- Optimize training for a specific TWSME actuator application
- Use the same training method to obtain different properties
- Can we apply this to the load-biased actuators??

# Neutron Diffraction at LANL

## (i) Experiment



## (ii) Model

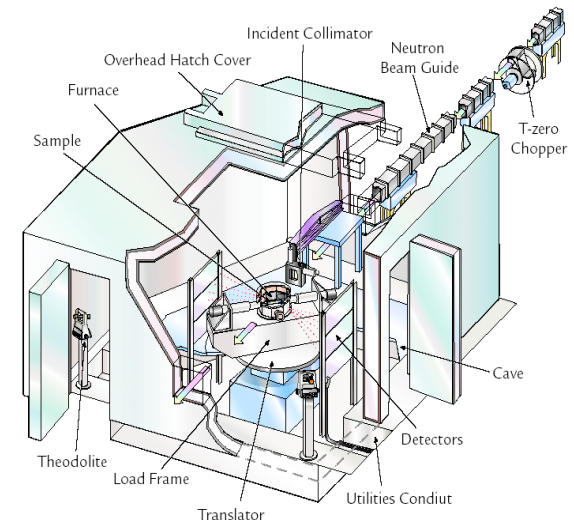
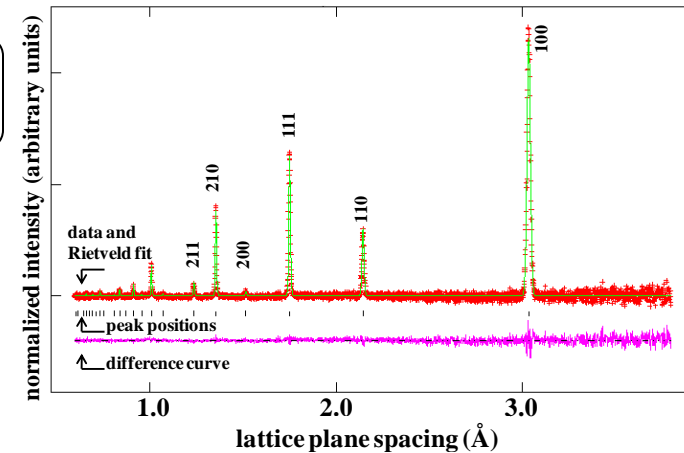
*Rietveld refinement*  
*multi parameter curve fitting*

$$Y_{ci} = Y_{bi} + s \sum_k L_k |F_k|^2 \phi(2\theta_i - 2\theta_k) P_k A$$

$Y_{bi}$ : background intensity  
 $s$ : scale factor  
 $L_k$ : Lorentz factor a  
 $F_k$ : structure factor  
 $f$ : refraction profile function  
 $2\theta_i$ : observed Bragg peak position  
 $2\theta_k$ : corrected calculated Bragg peak position  
 $P_k$ : preferred orientation function  
 $A$ : absorption factor

- Bulk penetration ~1cm
- Ability to follow micromechanical and microstructural changes
- Phase specific, quantitative information during heating/cooling and loading
- **Material: 55NiTi (wt%), d = 5.08 mm**

## (iii) Result



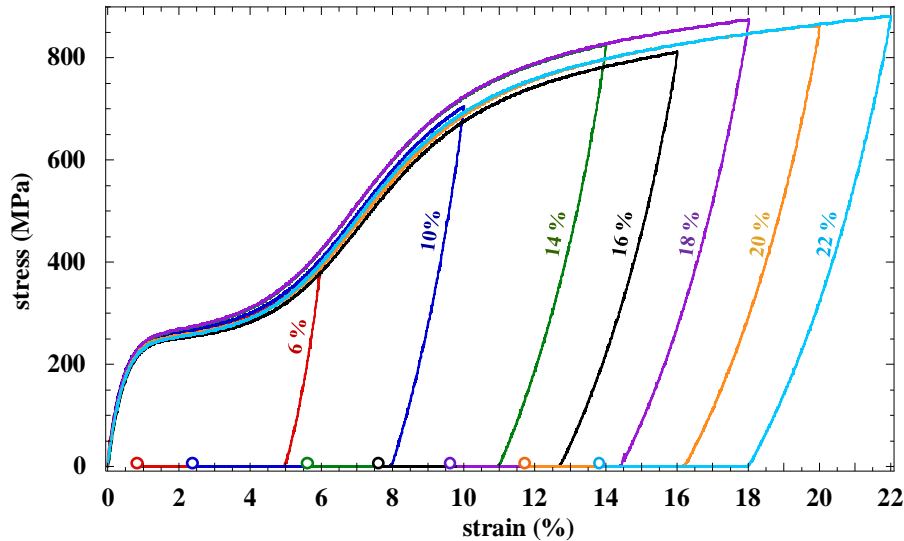
Spectrometer for Materials Research at Temperature and Stress (SMARTS)



# Training Procedures

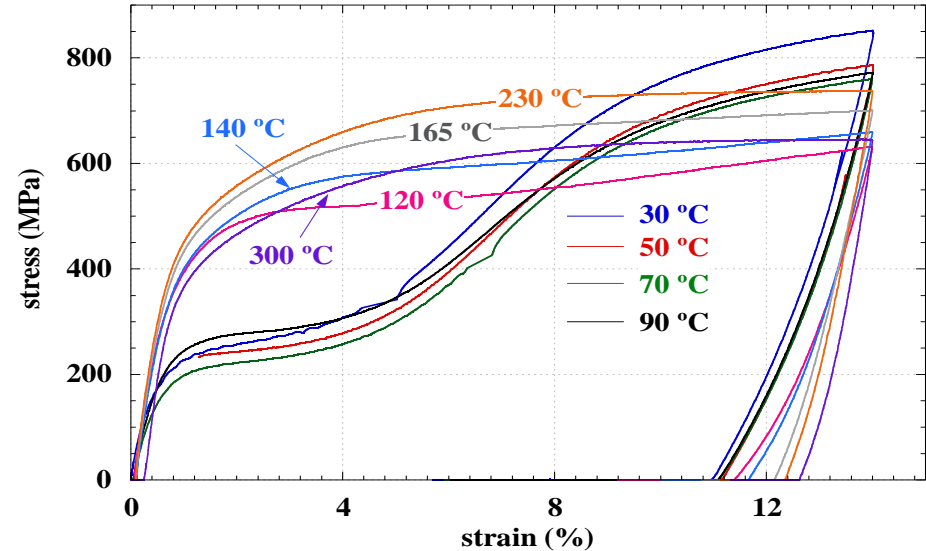
## Training I

Constant temperature  
Variable strain

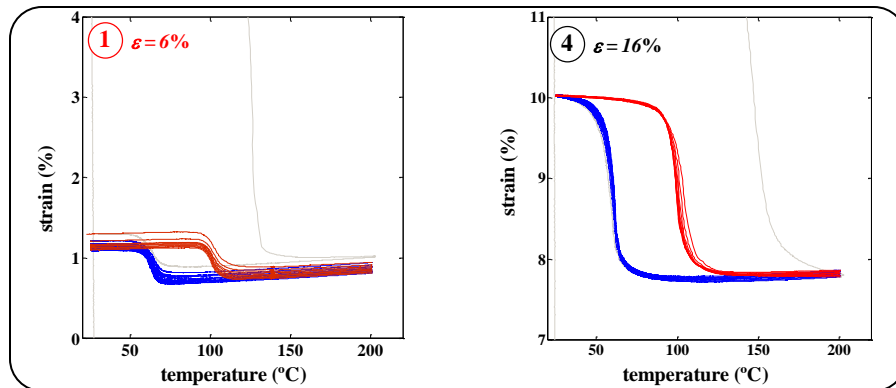


## Training II

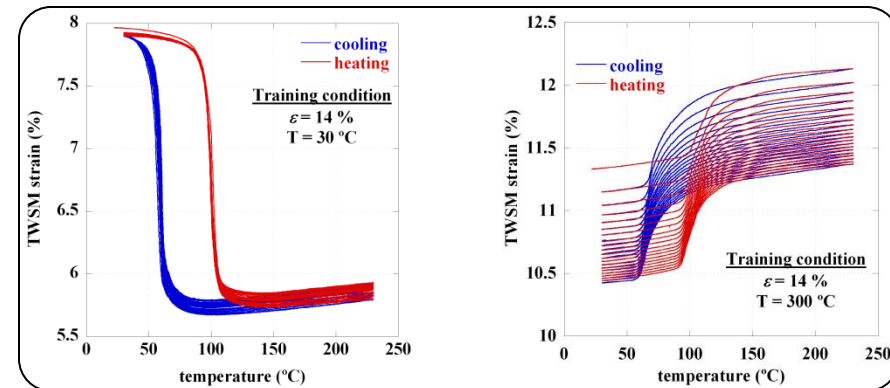
Constant strain  
Variable temperature



## No-load thermal cycling (TWSME)



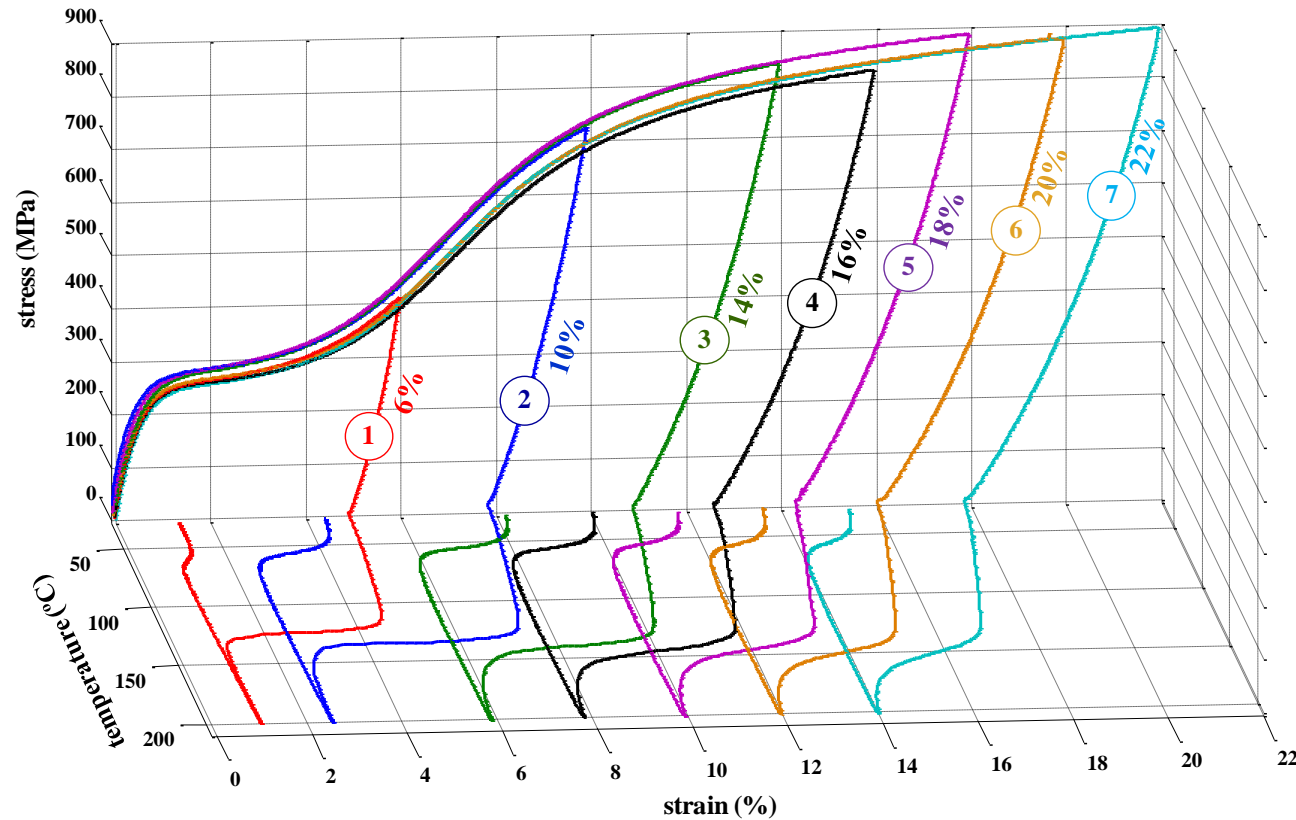
## No-load thermal cycling (TWSME)



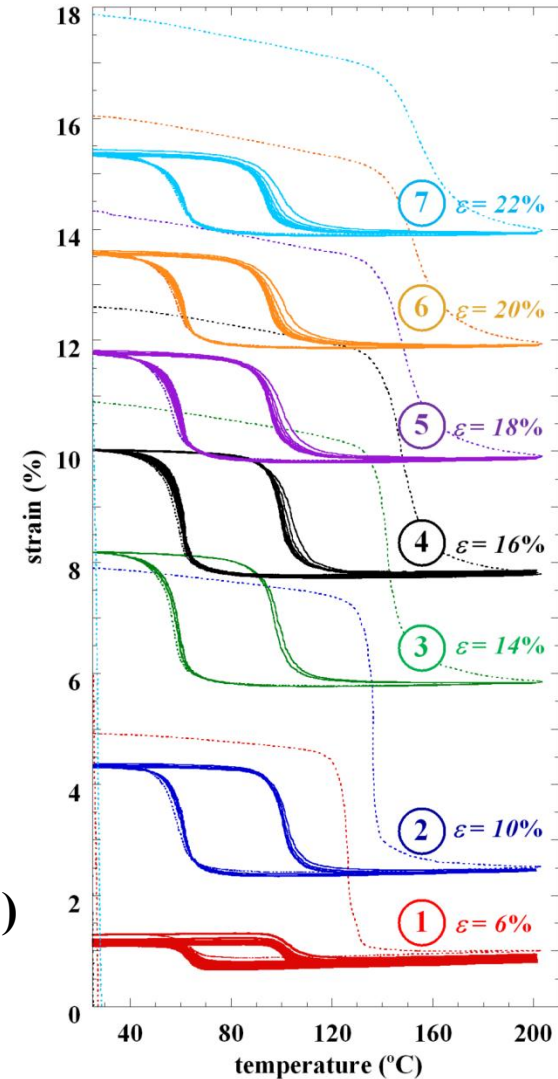


# Training I: Constant Temperature/Variable Strain

## Isothermal deformation



## TWSME



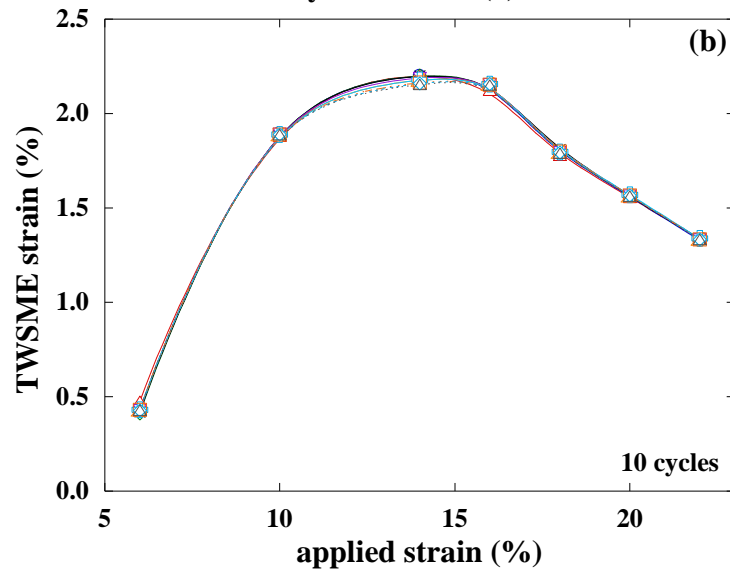
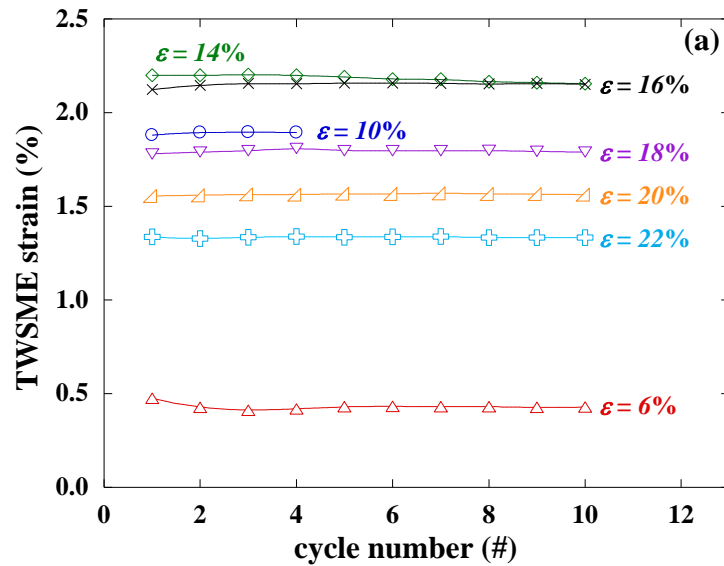
- Room temperature deformation in strain control ( $1 \times 10^{-4} \text{ sec}^{-1}$ )
- No-load thermal cycling ( $30 \leftrightarrow 200 \text{ }^{\circ}\text{C}$ )



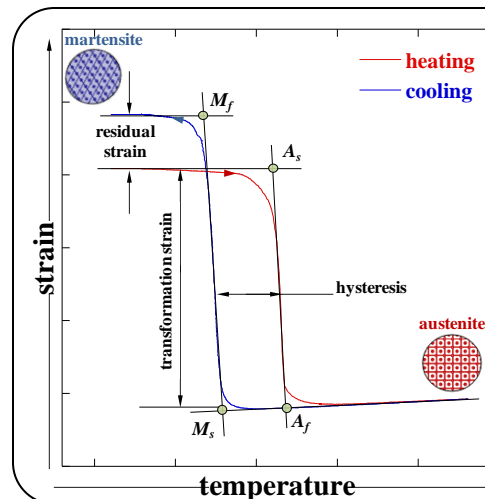
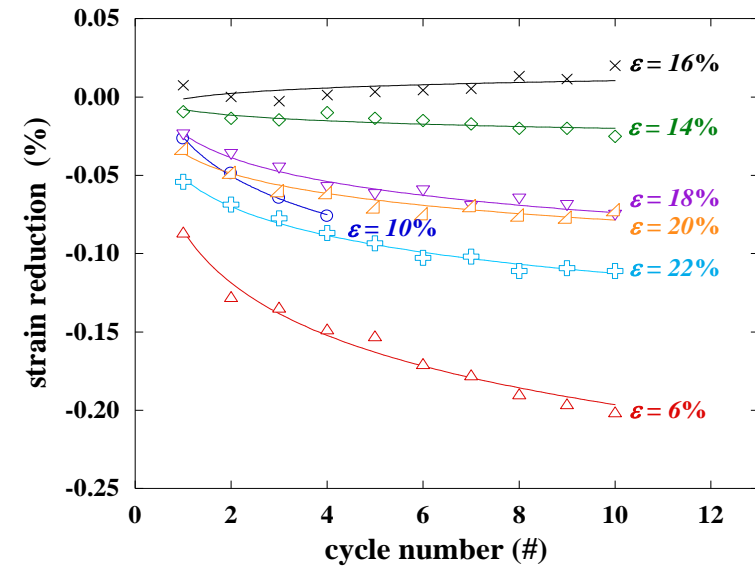


# Training I: Constant Temperature/Variable Strain

## TWSME magnitude



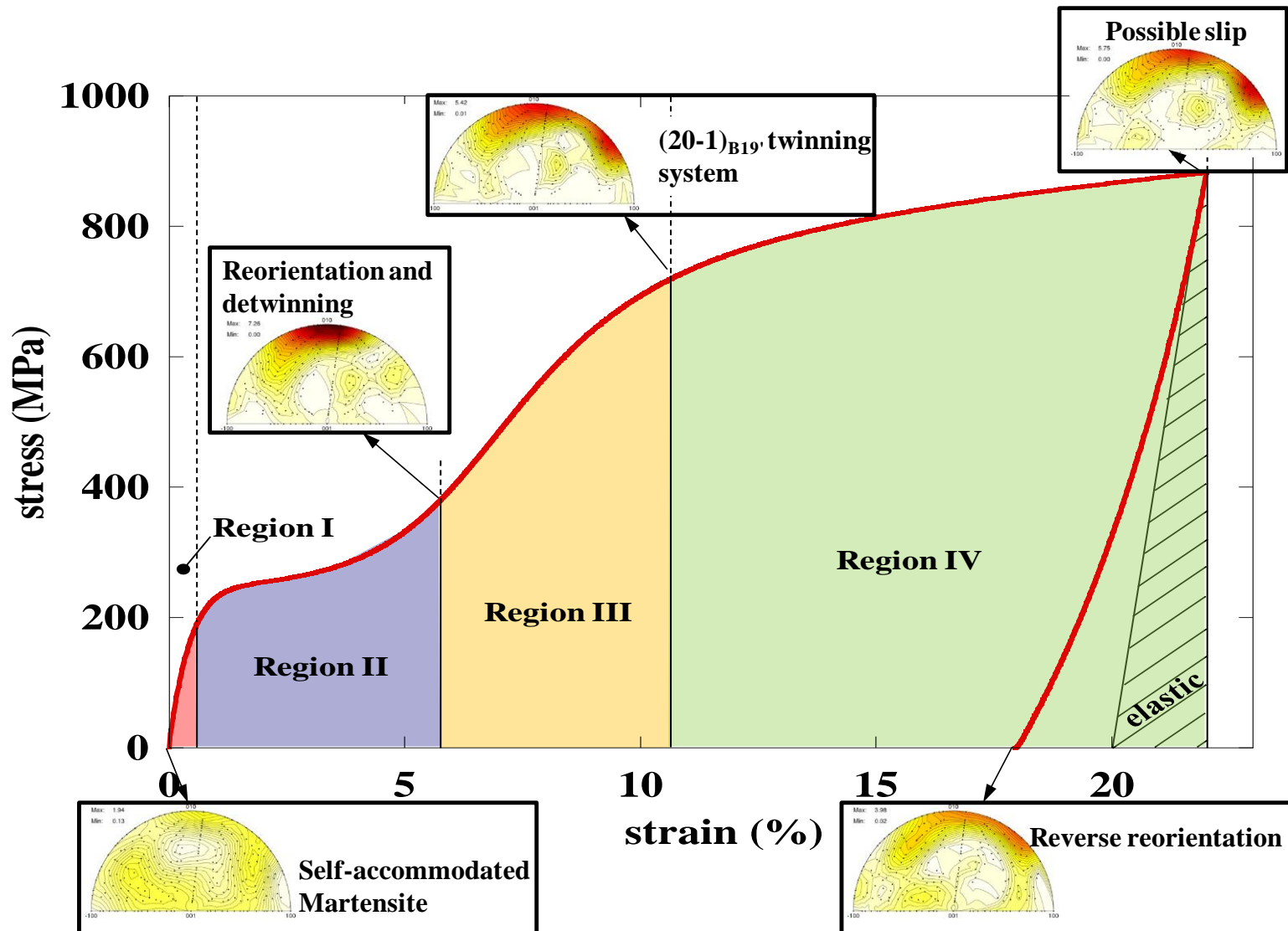
## TWSME stability



- Straining to 14 - 16% was found to be optimum for this material
- Stable TWSME strain of 2.2% was obtained with near-zero strain reduction
- Why 14-16%?



# Deformation Mechanisms in Martensitic NiTi

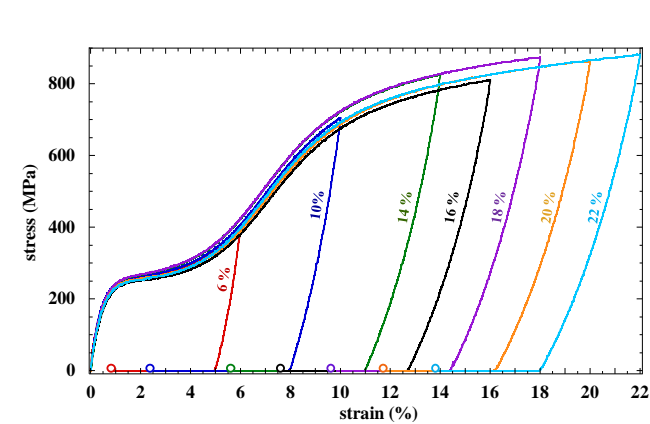
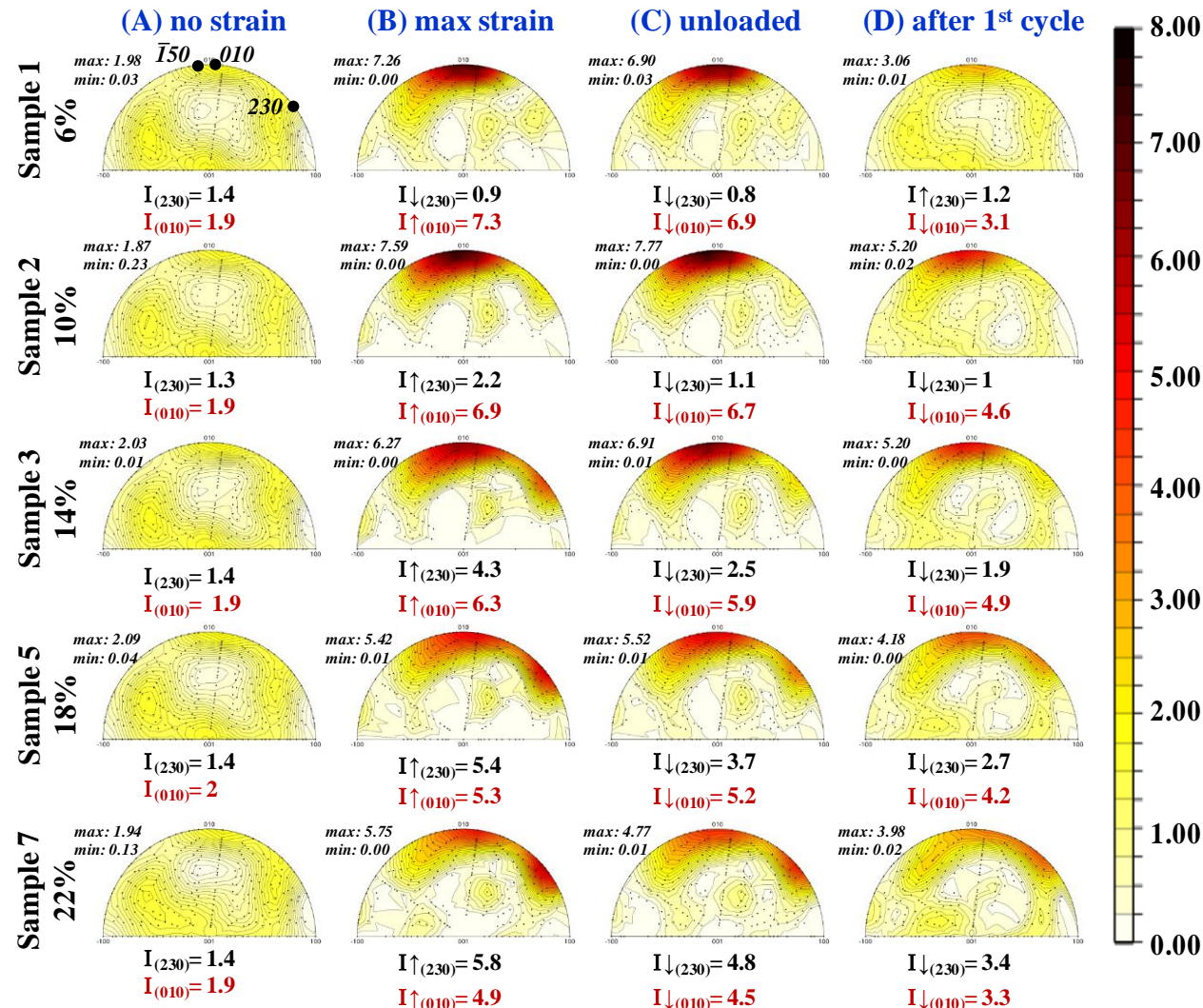




# Training I: Constant Temperature/Variable Strain

## Microstructure

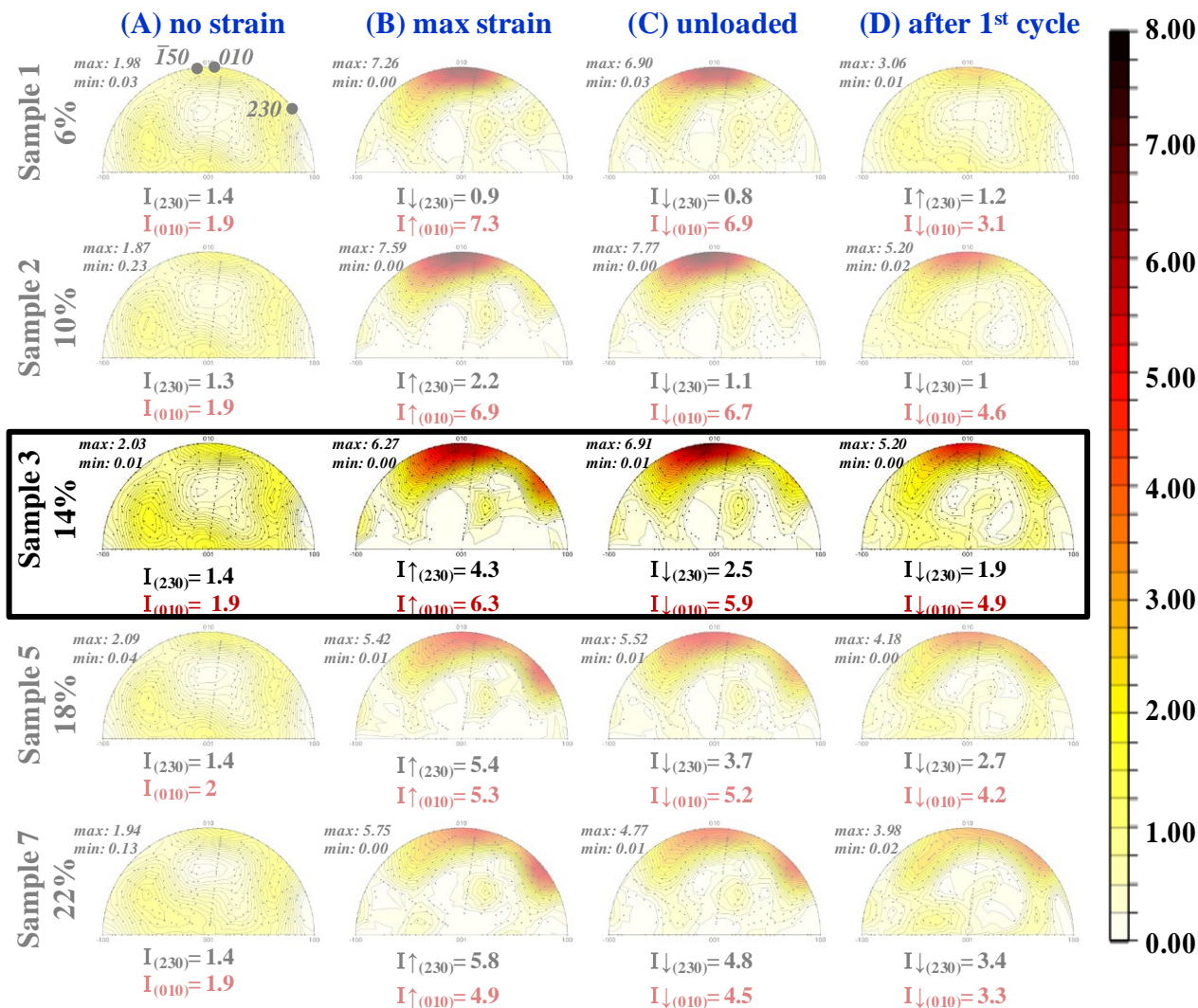
## Macroscopic response



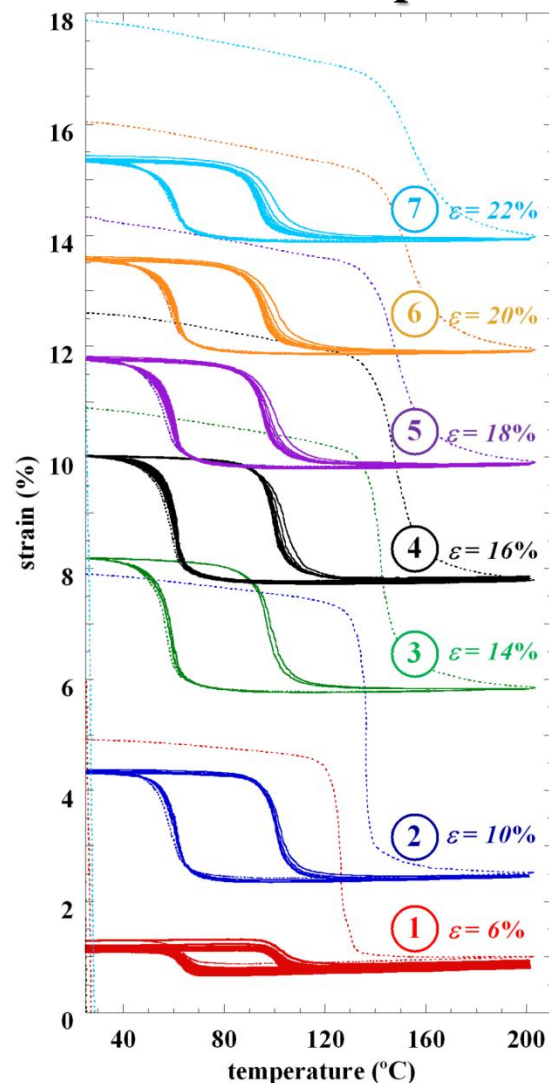


# Training I: Constant Temperature/Variable Strain

## Microstructure



## TWSME Response

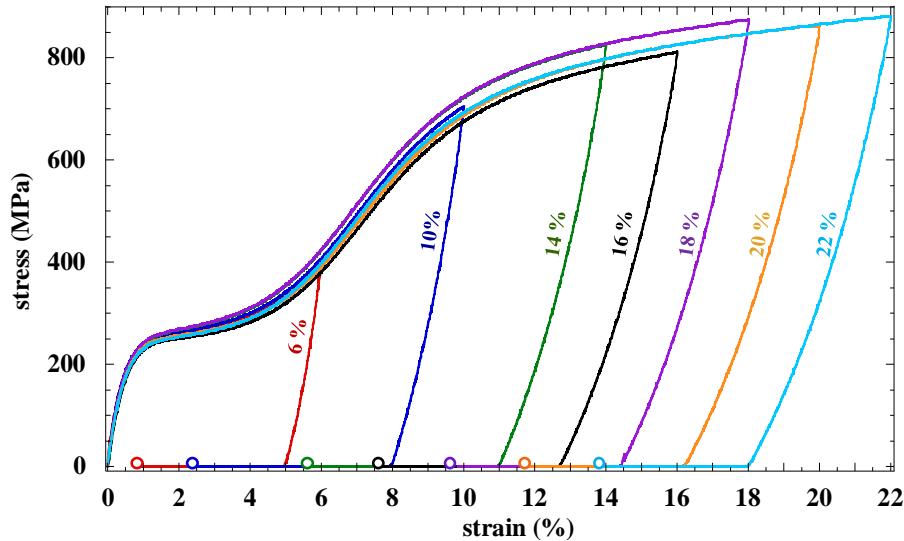




# Training Procedures

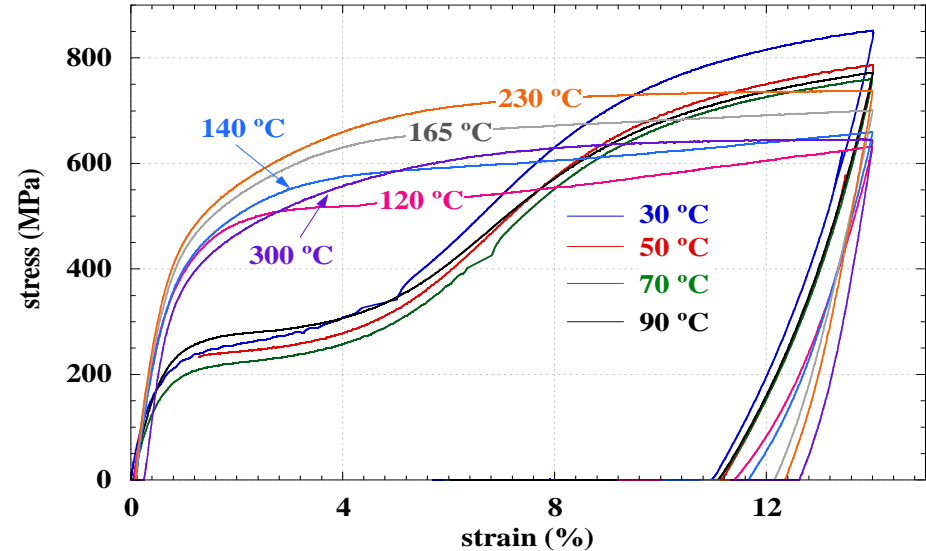
## Training I

Constant temperature  
Variable strain

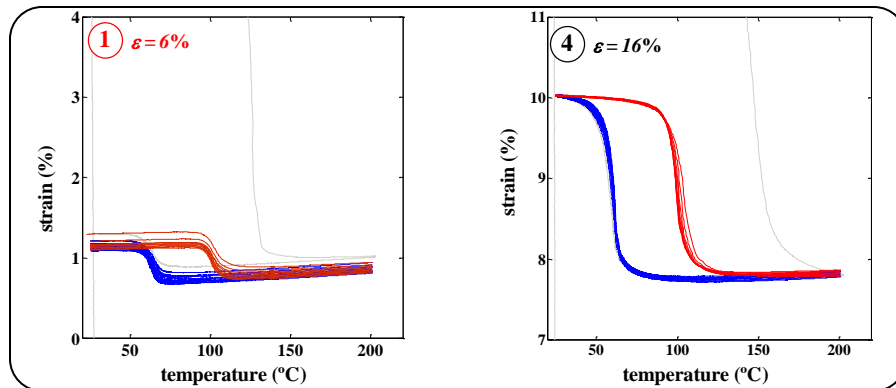


## Training II

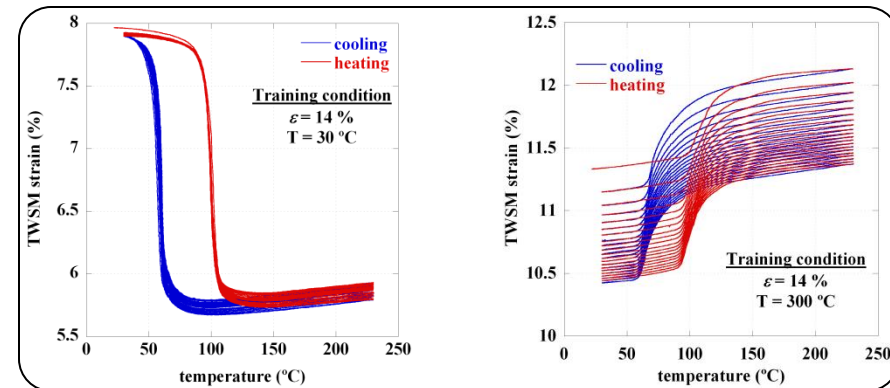
Constant strain  
Variable temperature



No-load thermal cycling (TWSME)



No-load thermal cycling (TWSME)

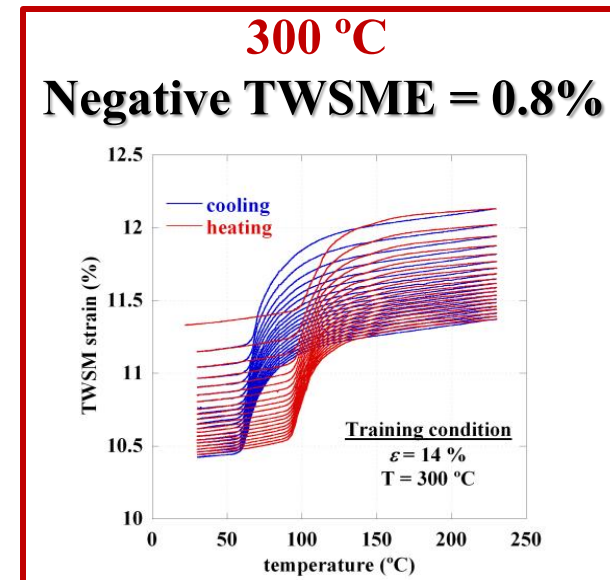
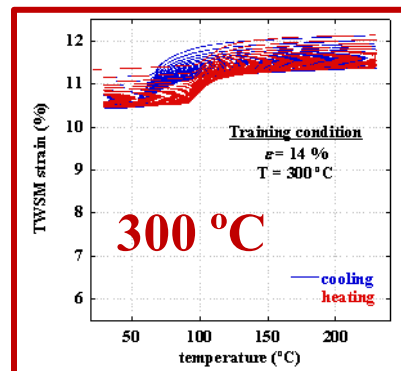
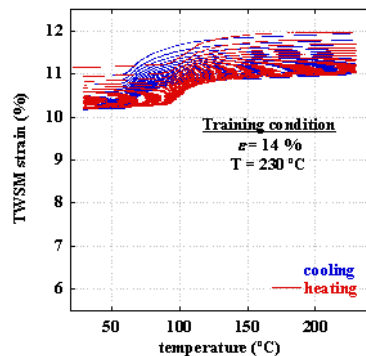
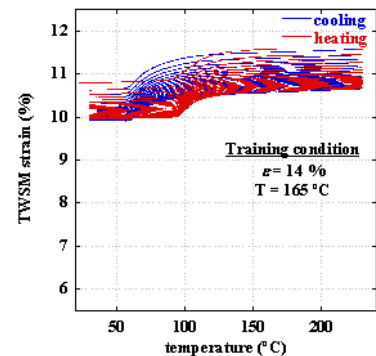
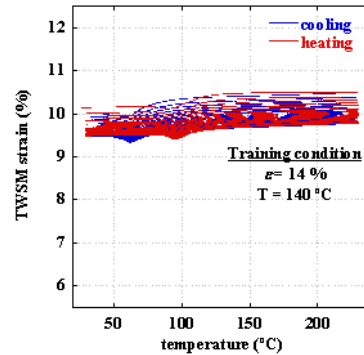
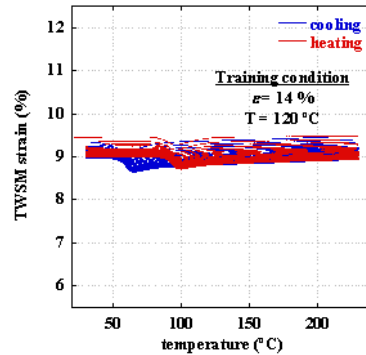
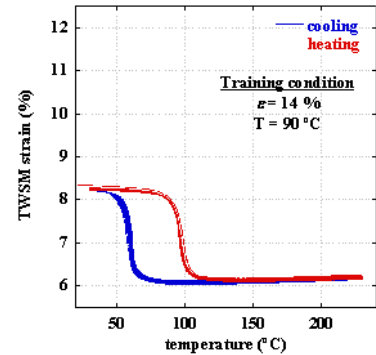
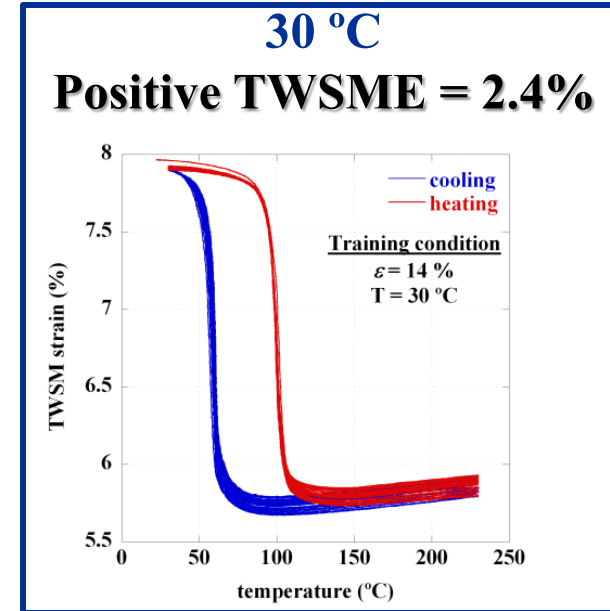
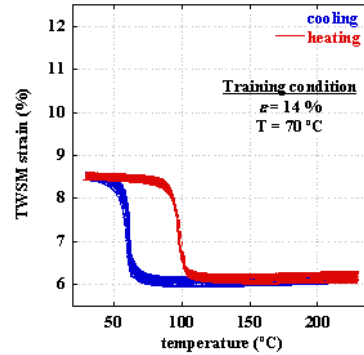
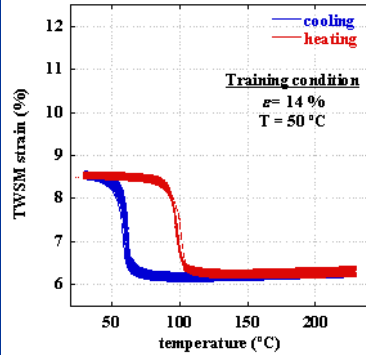
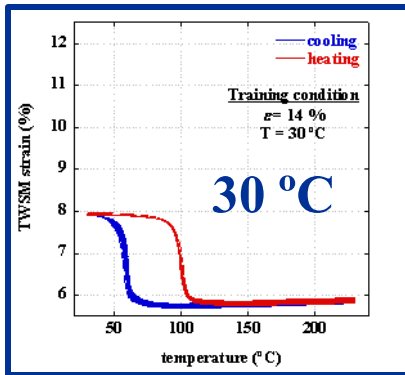






# Training II: Constant Strain/Variable Temperature

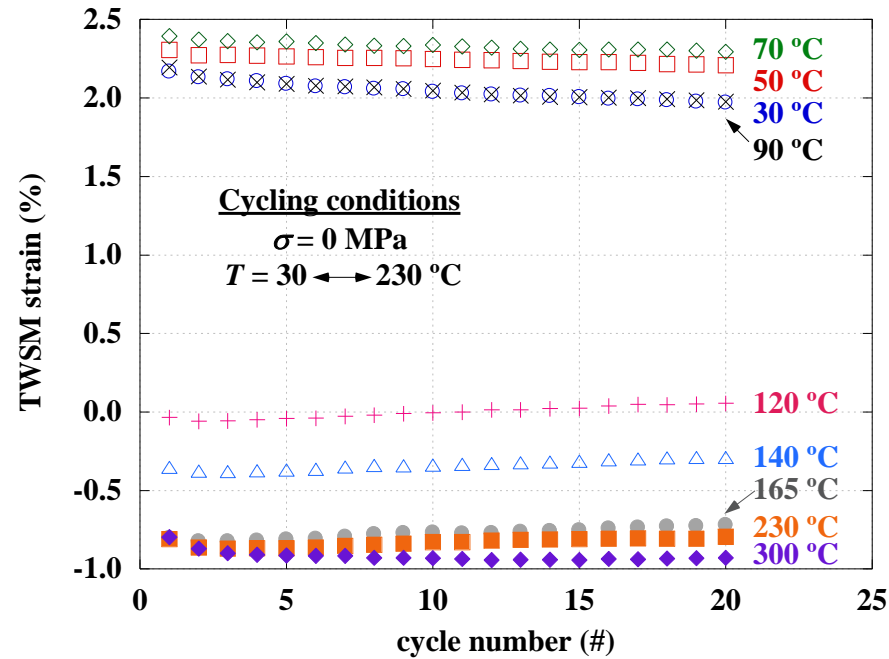
## TWSME Response



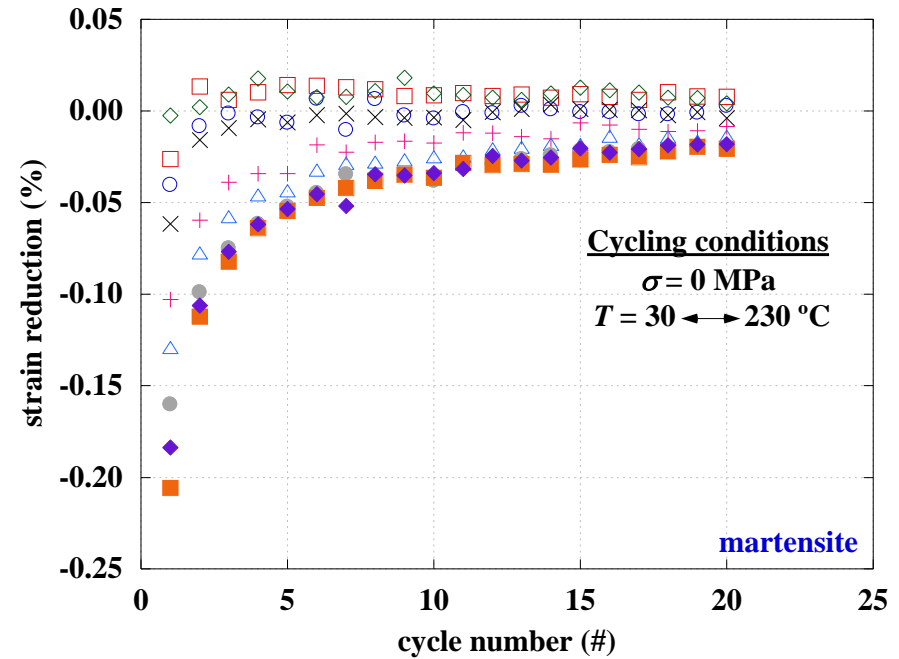


# Training II: Constant Strain/Variable Temperature

## TWSME magnitude



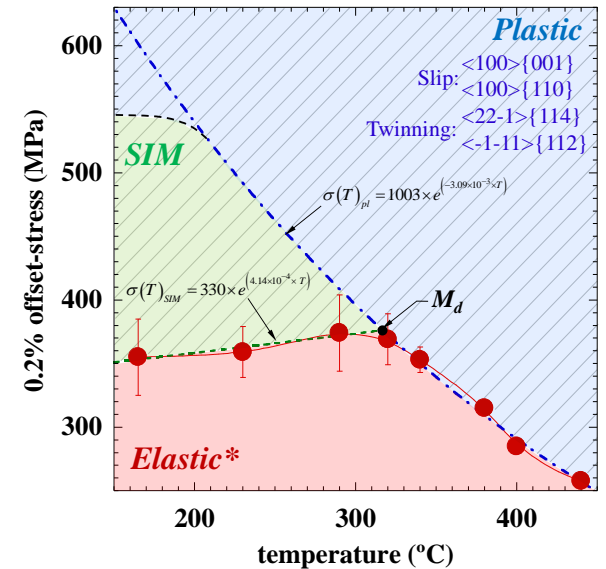
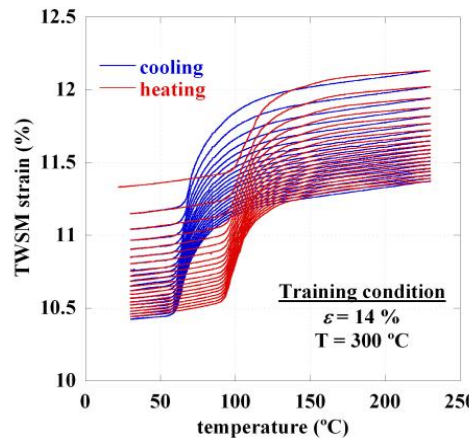
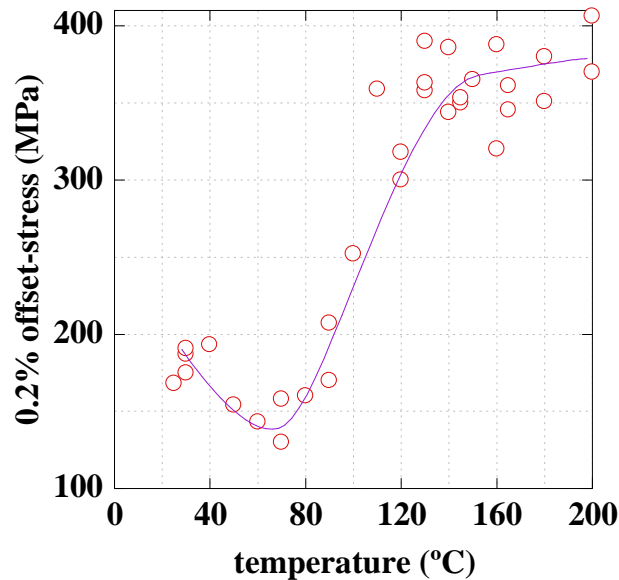
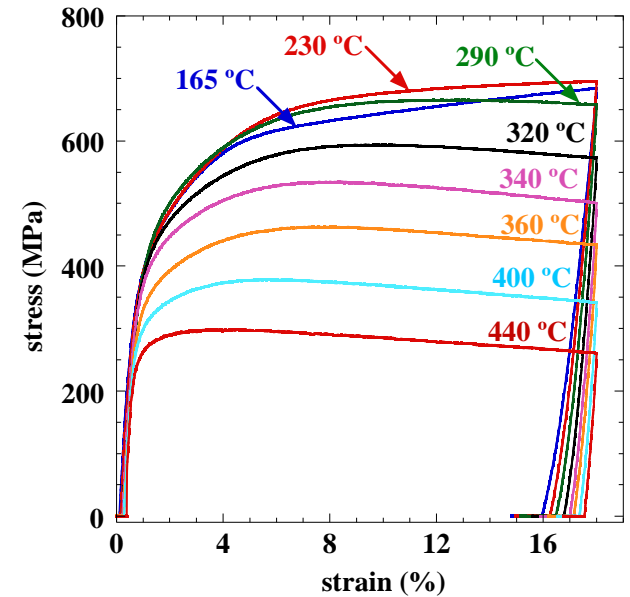
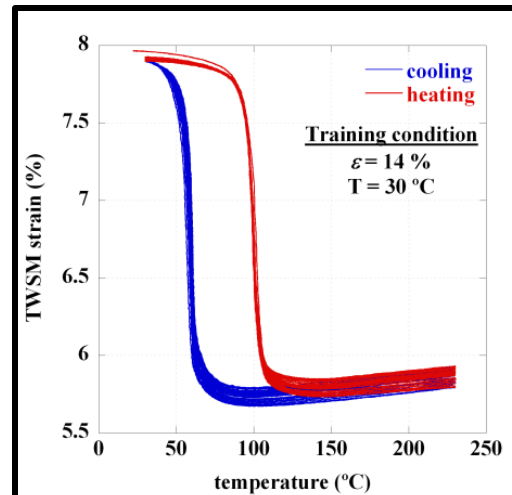
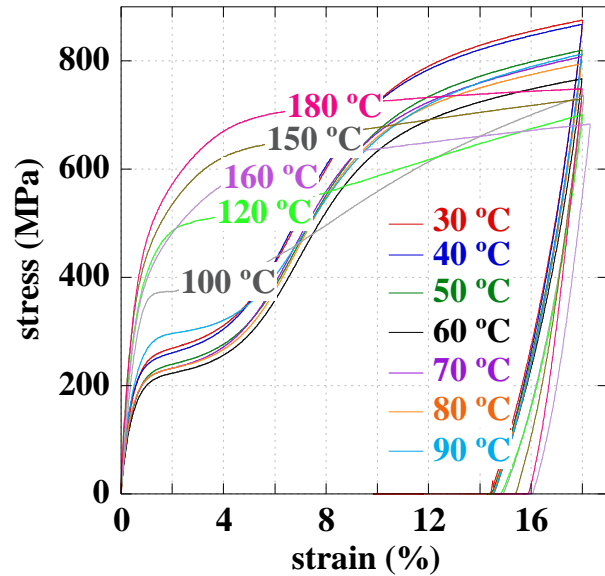
## TWSME stability



- Positive TSWME  $\rightarrow \sim 2.4\%$
- No TWSME  $\rightarrow 0\%$
- Negative TWSME  $\rightarrow \sim -1\%$



# Training II: Constant Strain/Variable Temperature

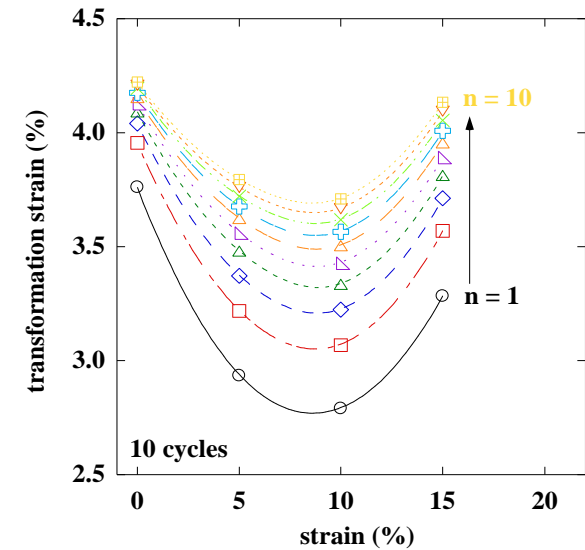
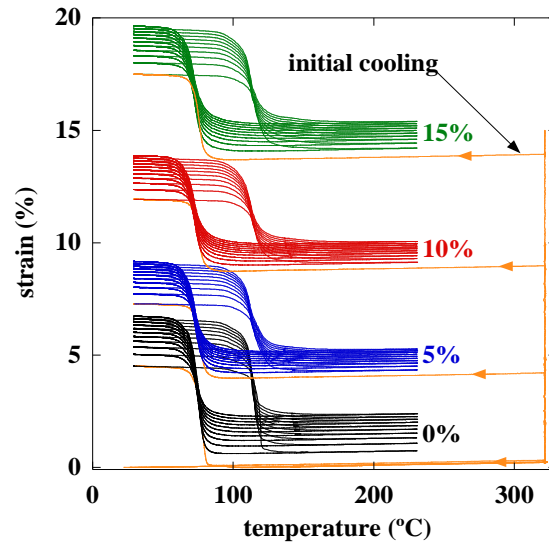
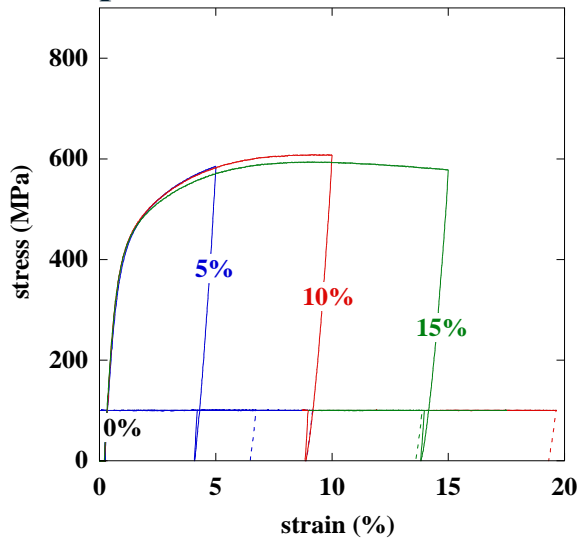




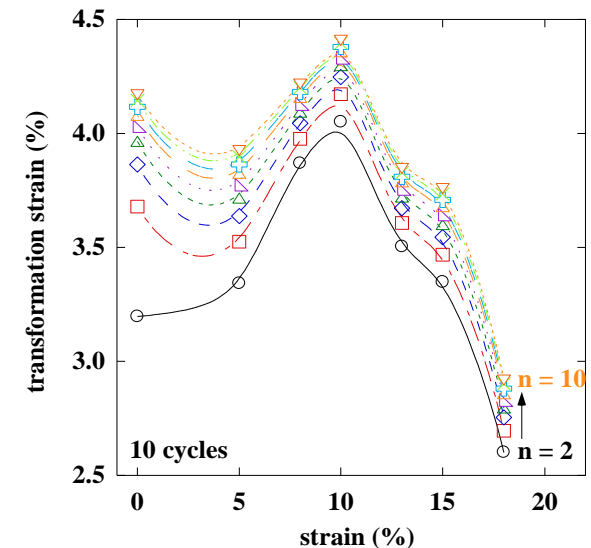
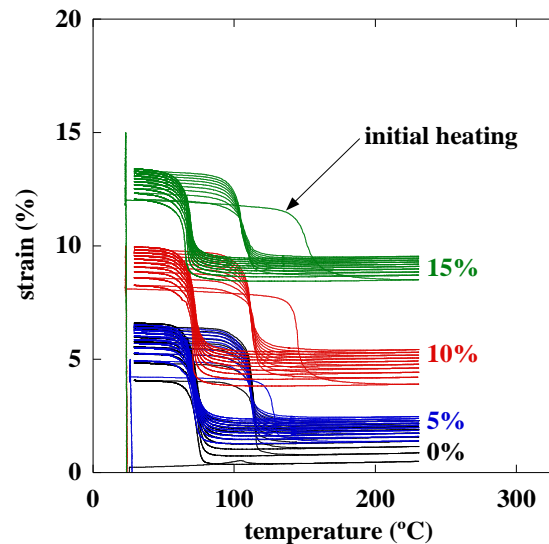
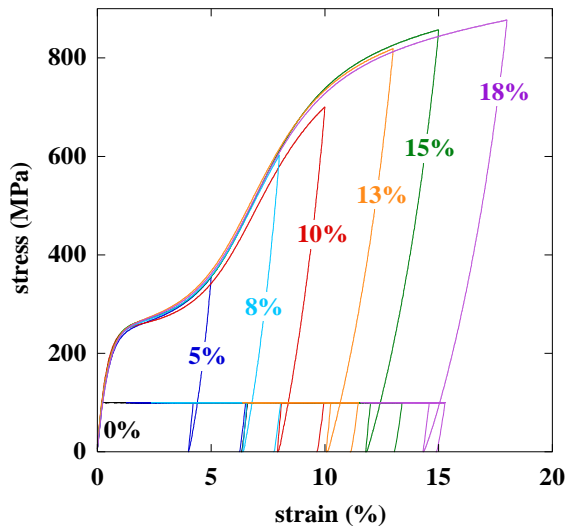


# Extend from TWSME to Load-Biased On the Optimization of Actuator Properties

Samples deformed at 320 °C



Samples deformed at RT





# Summary and Conclusions

- **The role of deformation and the corresponding microstructure on the TWSME training was investigated**
- **The TWSME can be optimized to fit several applications using the same training procedure**
- **In this alloy (55NiTi):**
  - **Positive TSWME  $\rightarrow \sim 2.2\%$**
  - **No TWSME  $\rightarrow 0\%$**
  - **Negative TWSME  $\rightarrow \sim -1\%$**
- **Can be extended to optimize SMA actuators under load**
- **Understanding the microstructure (in this work using neutron diffraction) is key in training and optimizing the structure (e.g., SMA actuators)**